Utilization of Stone Waste in the Development of Value Added Products: A State of the Art Review

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Abstract

The utilisation of stone waste, in the form of mineral admixture as a pozzolanic and non-pozzolanic material for mortar and concrete has received considerable attention in recent years. This interest is part of the widely spread attention directed towards the utilisation of wastes and industrial by-products in order to minimise Portland cement (PC) and sand consumption, the utilisation of which being environmentally damaging. Another reason is that mortar and concrete, which contain pozzolanic as well as non-pozzolanic materials, exhibit considerable enhancement in durability properties. This paper reviews work carried out on the use of stone waste as a partial non-pozzolanic replacement for sand in mortar and concrete and in the containment of hazardous wastes. The literature demonstrates that different stone wastes is an effective inert filler which causes great improvement in the pore structure and hence the resistance of the concrete to the action of harmful solutions.

Keywords: Stone waste; Stone cutting industry; Slurry disposal; Environmental management; Mechanical property

1. Introduction

Stone, one of the most common building material of ancient times, is an ubiquitous material. A sustainable growth in the consumption of stone is observed all over the world in the recent years. Various types of stone such as granite, marble, limestone, slate etc. are used in construction purposes. The country wise production of stones is show in Fig.1 [1].

There is continuous increment in the demand of various types of stone which leads to enormous increase in the business of stone sector industry. Today, different operations on stones, like- quarrying, sawing, cutting etc. are being processed by modern technologies which are improving the rate of production of stones as well as stone waste continuously. The stone waste is now-a-days a serious environment problem which is threat to modern civilization. As it is a non-biodegradable material, therefore poses numerous hazards. If this stone waste is dumped on land then, it can reduce the rate of rain water percolating and deteriorate the soil fertility. Stone waste dumped in rivers, streams and seas contaminates the water and marine [2]. Although land-filling can be an alternative to reuse stone waste but apart from this, it can also be used to make various cement composites, as one of the best solution for disposing of stone waste, due to its economical and ecological advantages (2-6).

An immense work has already been done on the use of stone waste in the production of Self-compacting concrete (SCC), Bricks, Mortar, Tiles, Cement concrete as aggregate and filler (7-12). The aim of the application of cutting and polishing stone waste in cementitious system is to improve the characteristics of the fresh and hardened material. Stone waste has a filler effect by filling up the voids between the sand grains. With the proper grading, the higher packing density results in improvement of strength (Compressive strength, Tensile strength, Flexural strength), Durability issues, Abrasion resistance with decrement of Coefficient of permeability and Chloride ion penetration by formation of dense microstructure (13-20).
This paper reviews the engineering properties of stone waste, fresh and hardened properties and durability performance of cement mortar and concrete containing stone waste in the production of different construction materials.

2. Generation of stone waste

In general there are two types of waste named as quarry/cutting/sawing from in-situ stone site and polishing waste from construction sites. During the processing of stone, the raw stone block is cut as demanded either into tiles or slabs of various thickness (usually 2 or 4 cm), using diamond blades. Water is showered on blades while stone blocks are cut into sheets of varying thickness, to cool the blades and absorb the dust produced during the cutting operation. The amount of wastewater from this operation is very large. It is not recycled as the water is so highly alkaline that, if re-used, it can dim the slabs to be polished. In large factories, where the blocks are cut into slabs, the cooling water is stored in pits until the suspended particles settle (sedimentation tanks), then the slurry is collected in trucks and disposed off on the ground and left to dry. This water carries large amounts of stone powder. The polishing operation is fully automated with the use of powdered abrasives that keep on scrubbing the surface of the stone until it becomes smooth and shiny. Water showers are essential to prevent overheating of the blades. Generation and type of stone waste is given below in Fig. 2 and 3:

3. Problems by dumped stone waste

In general, all the mines affect their surrounding environment to a little or more extent, but opencast mining i.e. in case of marble, granite, lime stone, sandstone and other type of building stone quarries leads to complex nature of environmental problems such as

(1) Choking of drains in rainy season
(2) Dust nuisance
(3) Fine particles of slurry (with size less than 363 micron) become air borne and cause air pollution
(4) Slurry affects productivity of land due to decreased porosity, water absorption and percolation
(5) Slurry dumped areas cannot support vegetation and remain degraded
(6) Due to long-term deposition of slurry on land, the finer particles block the flow regime of aquifers. Thus, seriously affecting underground water availability

So these waste material needs to be utilized meaningfully in an economic way.

4. Properties of stone waste

Different stone waste like granite, marble, limestone, sandstone etc. have different properties. However, a particular stone waste may have different physical and chemical properties depending on the method of generation of waste. It has been found that in cutting waste, calcium oxide (CaO) and in polishing waste, silicon-di-oxide (SiO₂) is the main constituent. The properties of some types of stone waste used as an aggregate in concrete are presented in Table 1 and 2. Table 3 indicates amount of substitution by stone waste in different proportions.
### Table 1: Physical and mechanical properties of powder and slurry stone waste

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Types of stone waste</th>
<th>Property</th>
<th>Specific gravity</th>
<th>Bulk density, (kg/m³)</th>
<th>Water absorption (%)</th>
<th>Max. particle size (mm)</th>
<th>Fineness modulus (FM)/Blaine fineness (cm²/g)*</th>
<th>Color</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Marble stone waste</td>
<td></td>
<td>2.12-2.67</td>
<td>1300-1500 (SL)</td>
<td>22-24(SL)</td>
<td>0.062 (Dry)</td>
<td>5100-5250*</td>
<td>White/ Dirty white</td>
</tr>
<tr>
<td>2</td>
<td>Lime stone waste</td>
<td></td>
<td>2.58-2.65</td>
<td>1568-1743 (SL)</td>
<td>2-4</td>
<td>0.2 (Dry)</td>
<td>3900-4123*</td>
<td>White/ Dirty white</td>
</tr>
<tr>
<td>3</td>
<td>Granite stone waste</td>
<td></td>
<td>2-2.84</td>
<td>1210-1465 (Dry)</td>
<td>26-28 (SL)</td>
<td>0.065 (Dry)</td>
<td>0.90-2.00(FM)</td>
<td>Pink to gray</td>
</tr>
</tbody>
</table>

SL-Slurry

### Table 2: Chemical properties of different stone waste

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Types of stone waste (Powder/Slurry)</th>
<th>Property</th>
<th>Chemical Constituent (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>Calcium Oxide (CaO)</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Silica (SiO₂)</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Aluminum Trioxide(Al₂O₃) + Ferrous Oxide (Fe₂O₃)</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Potassium Oxide + Sodium Oxide</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Magnesium Oxide (MgO)</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td>Loss on ignition (LOI)</td>
</tr>
</tbody>
</table>

### Table 3: Amount of substitution by Stone waste

<table>
<thead>
<tr>
<th>S.No.</th>
<th>Types of stone waste</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Concrete</td>
<td>Agarwal (2008)</td>
</tr>
<tr>
<td>2</td>
<td>Concrete</td>
<td>Al-Akhras et. al(2010)</td>
</tr>
<tr>
<td>3</td>
<td>Concrete</td>
<td>Alzboon et. al(2009)</td>
</tr>
<tr>
<td>4</td>
<td>Self-compacting concrete</td>
<td>Felekoglu et. al(2007)</td>
</tr>
<tr>
<td>5</td>
<td>Bricks</td>
<td>Gnanavel et. al(2009)</td>
</tr>
<tr>
<td>6</td>
<td>Self-compacting concretes</td>
<td>Gsog’lu et. al(2012)</td>
</tr>
<tr>
<td>7</td>
<td>Concrete bricks</td>
<td>Hamza et. al(2011)</td>
</tr>
<tr>
<td>8</td>
<td>Concrete</td>
<td>Alzboon et. al(2009)</td>
</tr>
<tr>
<td>9</td>
<td>Mortar</td>
<td>Agarwal (2008)</td>
</tr>
<tr>
<td>10</td>
<td>High strength lime binder</td>
<td>Agarwal (2008)</td>
</tr>
<tr>
<td>11</td>
<td>Concrete</td>
<td>Al-Akhras et. al(2010)</td>
</tr>
</tbody>
</table>
4.1 Fresh concrete properties

**Slump value**

The slump is used to measure the workability of fresh concrete mix. Being an important property, the slump of concrete and cement mortar mix containing stone waste was studied extensively. In the majority of the studies, a lower slump value of fresh concrete due to the incorporation of several types of stone waste as compared to conventional concrete mix was observed and an increasing addition of stone waste further lowers the slump value. The reasons for the lower slump value of the concrete mix containing stone waste was the particle size of stone aggregate. In a few studies, an increase in the slump value due to the incorporation of stone waste was also reported, the increase of the slump of concrete mixes due to the incorporation of stone waste is due to the presence of more free water in the mixes containing stone waste than in the concrete mix containing natural aggregate.

The possibility of using marble powder (MP) and limestone filler (LF) in the production of self-compacting concretes (SCCs) with and without fly ash was investigated [21]. The results obtained showed that as lime stone waste content increased, slump flow diameter and T_500 mm slump flow time was decreased.

Use of burnt stone slurry (BSS) waste by replacement with silica in concrete mixtures was investigated and found that in case of mortar, workability decreased with increment of BSS content due to the low rate of reaction of the BSS compared to that of cement [22]. Also, the utility of quarry dust limestone powder (QLP) in self-compacting paste and concrete applications was investigated and it was concluded that the incorporation of QLP increased the viscosity of the cement paste at the same water/powder ratio and superplastizer dosage [23].

**Unit weight**

Irrespective of the type and size of substitutions, the incorporation of stone waste as aggregate generally decreases fresh and dry densities of the resulting concrete due to the fineness of stone waste aggregate [23-25]. The behavior of marble dust (MD) in self-compacting concrete (SCC), as filler material was studied [26]. The result obtained was that unit weight of SCC had decreased because of increase in air content. In ceramics studies, the effect of incorporation of granite and marble sawing powder waste up to 50 wt. % into the raw clay material used for brick manufacturing with the result that bulk density was increased as reject content increased at constant sintering temperature [27].

**Air content**

There is direct relationship between strength properties and air content. Each percent increase in air content can reduce compressive strength by 2% to 6% for moderate-strength concrete. Only few reports are available on the evaluation of air-content of cement mortar or concrete mixes containing untreated stone waste as aggregate. The behavior of marble dust (MD) in self-compacting concrete (SCC), as filler material was studied [26]. The result obtained showed that air content of SCC had increased by using marble dust in SCC.

**Setting time**

In case of mortar, initial and final setting time decreased with increment of burnt stone slurry (BSS) content due to the low rate of reaction of the BSS compared to that of cement. The results showed that addition of marble dust accelerate the setting. The results of initial and final setting times of control (OPC) and OPC blended with marble dust (20%, 40% and 60%) and rice husk ash (10%, 20% and 30%) are shown in Fig.4:
The possibility of using marble powder (MP) and limestone filler (LF) in the production of self-compacting concretes (SCC) with and without fly ash was investigated [21]. To observe the replacement levels of MP and LF, seven binary and six ternary blends of SCC mixtures apart from a control mixture were designed. The results were obtained showed that as stone waste content increased, initial and final setting times increased than that of controlled specimen by replacing cement.

4.2 Hardened concrete properties

Compressive strength
The compressive strength of concrete and cement mortar is a fundamental property that is thoroughly studied in almost all research works. Literature studies showed that the incorporation of stone waste such as limestone, marble and marble with granite stone waste etc. as an aggregate decreased the compressive strength of the resulting concrete/mortar with the replacement of cement due to less binding effect and increased with sand replacement due to filler effect [23, 24, 28-32].

The behavior of marble dust (MD) in self-compacting concrete (SCC), as filler material had been studied [26]. For this purpose, MD had replaced binder of SCC at certain contents of 0, 50, 100, 150, 200, 250 and 300 kg/m³. Compressive strength was determined at the end of 28 days for the hardened concrete specimens. It was found that the compressive properties of hardened SCC had decreased by using MD as shown in Fig. 5.

Experimental study to investigate the strength variation in concrete and mortar by replacement of sand with stone waste had been carried out as shown in Fig. 6 [33]. Compressive strength of mortar was found to 33.02 MPa at proportions of 1:2.75 which was 21% higher than conventional. The compressive strength of concrete was also observed 31MPa at proportions of 1:1.5:3 which was 14.76% higher than that of normal sand (26 MPa).
Splitting tensile strength

As shown in case of compressive strength, the incorporation of any type of stone waste decreased the tensile strength of the resulting concrete/mortar with the replacement of cement and increased with sand replacement. The tensile strength behavior of mortar containing various percentages of limestone waste (LSW) and marble powder (MP) are presented in Table 4[34].

<table>
<thead>
<tr>
<th>% (LSW)</th>
<th>% (MP)</th>
<th>$f_{sp,28}$ days (MPa) At cement content 350 Kg/m$^3$</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>0</td>
<td>3.7</td>
</tr>
<tr>
<td>0</td>
<td>15</td>
<td>4.1</td>
</tr>
<tr>
<td>50</td>
<td>15</td>
<td>4.5</td>
</tr>
</tbody>
</table>

The experimental study undertaken to investigate the influence of partial replacement of sand with limestone waste (LSW), with marble powder (MP) as an additive on the concrete properties was reported [35]. The replacement proportion of sand with limestone waste, 25%, 50%, and 75% were practiced in the concrete mixes. Besides, proportions of 5%, 10% and 15% marble powder were practiced in the concrete mixes. The result showed that tensile strength increases with the increment of lime stone waste.

Modulus of elasticity (E)

According to ASTM C 469, the modulus of elasticity is defined as a stress to strain ratio value for hardened concrete. The type of aggregate influences this modulus, since the deformation produced in concrete is partially related to the elastic deformation of the aggregate. The effect of stone waste on the behaviour of concrete’s modulus of elasticity is reported in some research paper.

The use of marble and granite (MGR) as a sustainable alternative for cement replacement was investigated [30]. Chemical analysis and particle size distribution showed that MGR was a non-reactive material and may act as filler. In this work, experimental research had been conducted where 5%, 10% and 20% of the cement was replaced by MGR. Elastic modules test was conducted to examine the mechanical performance of concrete containing MGR and results showed that $E$ decreased as % mixed waste increased at constant (w/c) ratio and also $E$ decreased as w/c ratio increased at constant % mixed waste. Mohamadien et al. reported the experimental study undertaken to investigate the influence of partial replacement of sand with limestone waste (LSW) and marble powder (MP) as an additive on the concrete properties. The replacement proportion of sand with limestone waste 25%, 50%, and 75% were practiced in the concrete mixes. Besides, proportions of 5%, 10% and 15% marble powder were practiced in the concrete mixes. The result showed that the modulus of elasticity increased with increasing the limestone waste with marble powder.

Flexural strength
Flexural strength is defined as the material’s ability to resist deformation under flexural load and is measured in terms of stress. It represents the highest stress experienced within the material at the collapse load.

Use of burnt stone slurry (BSS) waste by replacement with silica in concrete mixtures was investigated [22]. To make samples portland cement (Type I), natural silica sand, BSS and water were used. BSS was added to mortar mixtures as a partial replacement of the silica sand at three levels 5%, 10%, and 15% by weight. Curing of samples was done by both moist curing and autoclaving curing. It was noticed that up to 10% replacement the flexural strength increased. However strength by autoclave curing was more than moist curing due to the high temperature of autoclaving curing that leads to higher speed of hydration and consequently leads to higher concrete strength. This behavior of strength was due to high amount of lime in BSS which reacts with silica forming additional C-S-H gel which contributes to the increase in the strength. The behavior of marble dust (MD) in self-compacting concrete (SCC), as filler material was studied [26]. The result showed that flexural properties of hardened SCC had decreased by using Marble dust waste.

The utilization of waste marble dust as an additive material in industrial brick was investigated [35]. In general, the addition of waste up to levels of 10 wt.% did not play significant changes in the relevant functional characteristics, but when the amount of marble powder additives were increased, the physico-mechanical properties of bricks were increased remarkably. The results for this study showed that 10% by weight of marble powder can be added to an industrial brick mortar with no sacrifice of technical properties of the final product. Adding waste marble more than 10 wt. % decreased flexural strength drastically. Characterization laboratory tests on samples that were molded with different marble powder contents was carried out, fired at temperature varying from 750 to 950 °C. The results depicted the possibility of using this by-product in the paste composition of ceramic bricks [36]. It was found that at different temperature and different waste content the strength varies as shown in Fig.7.

![Fig. 7 Flexural strength with waste content](image)

4.3 Durability performance

Various durability factors evaluated for concrete or mortar containing stone waste consist of water absorption, sorptivity, shrinkage, carbonation resistance, chloride ion permeation and resistance against freezing and thawing which are described below:

**Permeability behaviour**

Generally the permeability of aggressive chemical species through the pores of concrete is the major factor that controls several durability properties. Tests like water absorption, gas permeability and chloride permeability measurement can provide information on the vulnerability of concrete to the ingress of deleterious chemical species.

**Capillarity property**

The behavior of marble dust (MD) in self-compacting concrete (SCC), as filler material was studied [26]. For this purpose, MD had replaced binder of SCC at certain contents of 0, 50, 100, 150, 200, 250 and 300 kg/m³ and the result obtained are
given in Fig. 8. The capillarity property of hardened SCC had increased by using Marble dust waste in large amount i.e. above 150 kg/m³. The utilization of marble waste of different sizes in the manufacturing of concrete bricks, with full replacement of conventional coarse and fine aggregates with marble waste scrapes and slurry powder of content up to 40% was studied [37]. The test result about water absorption is shown in Fig. 9 that qualifies them for use in the building sector.

![Fig. 8 Variation of capillary coefficient related to filler content](image1)

![Fig. 9 Water absorption for marble slurry samples](image2)

The use of waste marble dust as an additive material in industrial brick was studied [35]. Waste material in different proportions was mixed with industrial brick mortar starting amount from 0 to 80 wt. %. Archimedes water displacement test was conducted with different water absorption percentage values at 900, 1000 and 1100°C temperatures. From Fig. 10 it can be seen that the porosity values of waste mixed bricks increased with the increasing waste. One of the reasons of this result is the CaO mineral in the waste marble.

![Fig. 10 Water absorption with increasing amount of waste additives in brick compositions](image3)

**Porosity**

Voids in concrete can be filled with air or water. Air voids are obvious and easily-visible example of pores in concrete. Broadly speaking, the more porous the concrete, the weaker it will be. Probably the most important source of porosity in concrete is the ratio of water to cement in the mix. The use of powdered marble by-product to enhance the properties of brick ceramic, fired at temperature varying from 750 to 950°C and mechanical properties were evaluated [36]. The result obtained showed that at 15% replacement of stone waste the open porosity was less, as shown in Fig. 11.
Use of burnt stone slurry (BSS) waste by replacement with silica in concrete mixtures was investigated [22]. To make samples portland cement (Type I), natural silica sand, BSS and water were used. BSS was added to mortar mixtures as a partial replacement of the silica sand at three levels i.e. 5%, 10% and 15% by weight. Curing of samples was done by both moist curing and autoclave curing. The moist cured mortar had higher degree of porosity in comparison with the autoclaved mortar. This behavior was due to the effect of autoclaving curing that produced more packing structure of mortar specimens compared to the moist curing. In this area, The usability of waste marble dust as an additive material in industrial brick was investigated [35]. Waste material in different proportions was mixed with industrial brick mortar starting amount from 0 to 80 wt. %. Sintering at three different temperatures 900, 1000 and 1100°C was done and the result showed that there is increase in porosity with the increasing amount of marble powder.

**Chloride ion permeability and electrical resistivity**

The possibility of using marble powder (M) and limestone filler (LF) in the production of self compacting concrete (SCC) with and without fly ash was investigated [21]. Rapid chloride permeability, electrical resistivity and sorptivity properties of SCC were determined at 90 days of curing. The results obtained showed that with the increase of limestone waste, chloride ion permeability decreases whereas electrical resistivity increases.

**Shrinkage**

The use of the powder marble by-product to enhance the properties of brick ceramic was studied [36]. It has been observed that the specimens fired at 850° C and 950 °C have shown similar behavior, where a very small decrease of linear variation between 0% and 5% of waste content was noticeable. The result obtained showed that at lower temperature of sintering the linear shrinkage was less as compared to other higher temperatures as shown in Fig. 12:
Use of burnt stone slurry (BSS) waste by replacement with silica in concrete mixtures at three levels 5%, 10%, and 15% by weight was investigated [22]. The results obtained are shown as follows in Fig. 13.

- Expansion in case of moist curing was more than that of autoclave curing
- In case of moist curing as % BSS increased, expansion was also increased
- In case of autoclave curing expansion at 10% replacement was same as that of 0% replacement

The changes in the physical and mechanical properties of the produced ceramic tiles from raw materials containing marble sludge slime produced in the ornamental stone processing industry was investigated [38]. The replacement of all the bentonite by sludge slime significantly decreased the shrinkage values of the tiles from 1.66% to 0.5%. The results showed that all of the produced sludge slime can be consumed successfully in ceramic production.

5. Practical implications

The above discussion proves that the incorporation of stone waste as replacement of sand in cement composites can improve various properties such as strength (compressive/tensile/flexural), thermal resistance, abrasion resistance, shrinkage, cracking increases which can solve a part of the problem associated with stone waste disposal. The practical implications of the results till date are given below in Fig. 14.

6. Conclusions
From the literature studies, it can be inferred that stone waste can be utilized for developing low cost building materials such as block, brick, tiles etc., however following studies are also recommended for utilizing this waste as an effective replacement of sand:

- Stone cutting powder with fly ash/rice husk ash/ ground granulated blast-furnace slag (GGBS) in cement concrete as mineral admixtures for the development of low cost building materials
- Development of lightweight block/panel for thermal and acoustic insulation purpose
- Study of lime stone waste as sustainable fillers in polymer matrices
- Microstructural study of different inorganic matrix with stone waste

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References


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