

Inner Current Loop with Closed Loop Speed Control of SEDC Motor Using Three Phase Fully Controlled Bridge Rectifier

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Abstract— The speed control of independently energized DC [SEDC] engines by PI and PID controller is broadly utilized as a part of industry application. This paper depicts the outlining of a shut circle model of the SEDC drive for controlling pace beneath the appraised speed. The numerical displaying of shut circle speed control of SEDC engine utilizing three stage completely controlled rectifier is finished. In this paper, the plan of PI speed controller utilizing modulus embracing approach for shut circle speed control of dc engine utilizing three stage completely controlled rectifier is exhibited. After that the Simulink model of rectifier sustained SEDC engine is made in Matlab. The outcomes are acquired for reference speed which is appraised or underneath the evaluated speed of engine. The speed of the engine is acquired at pre-set esteem [ref. Speed]. At the point when the heap is increment, speed of the engine is diminish. Yet, by shut circle control of engine, the speed of the engine is settled at reference speed.

Keywords: Fully controlled rectifier as a Converter, Modulus Hugging Approach, PI- Controller, SEDC Motor, and Simulink

I. INTRODUCTION

The speed of independently energized DC [SEDC] engine can be controlled underneath the evaluated speed by utilizing controlled rectifier as a converter. The controlled rectifier terminating circuit gets signals from the controllers and after that controlled rectifier gives variable voltage to the armature of the dc engine for accomplishes required speed. There are two control circles, initial one for controlling present and another for control of speed. Relative Integral [PI] sort controllers are utilized, which expels the postponement and gives quick control. [1][8]. In this paper at first scientific examination of SEDC engine is performed trailed by outlining of current and speed controllers. At that point modulus embracing approach is utilized to configuration speed controller. At last reproduction show is produced to get the outcomes.

II. EQUIVALENT CIRCUIT OF SEDC MOTOR AND EQUATIONS

The equivalent circuit of SEDC motor is given as:

Where: V_a is the armature voltage in volts.

: I_a is the armature current in amps.

: R_a is the armature resistance in ohms.

: L_a is the armature inductance in henrys.

: E_b is the back emf in volts.

: V_f and I_f is the field voltage and current respectively.

The armature voltage equation is given as:

$$V_a = I_a R_a + L_a \frac{d I_a}{dt} + E_b \quad (2.1)$$

The developed torque is given as:

$$T_d = J \frac{d\omega}{dt} + B\omega + T_L \quad (2.2)$$

Where:

- T_d is the developed torque in the motor in Nm.

- T_L is the load torque in Nm.

- J is the moment of inertia in Kg/m².

- B is the friction coefficient of the motor.

- ω is the angular velocity of motor in rad/sec.

Let assume that $B=0$, then

The developed torque is given as:

$$T_d = J \frac{d\omega}{dt} + T_L \quad (2.3)$$

The back emf of the motor will be:

$$E_b = K \omega \quad (2.4)$$

Where: K is the back emf constant in volt-sec/rad.

The developed torque is also given as:

$$T_d = K \phi I_a \quad (2.5)$$

After taking the Laplace Transform of above equations and the simplified equations:

The armature current is obtained as:

$$I_a(s) = \frac{V_a - E_b}{R_a (1 + T_a s)} \quad (2.6)$$

The equivalent circuit of SEDC motor is given as:

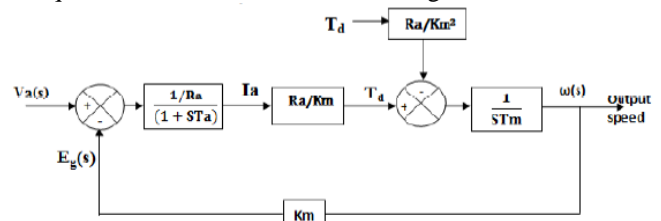


Figure2. Block model of SEDC motor.

III. REPRESENTATION OF THREE PHASE FULLY CONTROLLED RECTIFIER

Let the converter is a three phase fully controlled converter for a typical firing angle $\alpha = 60$.

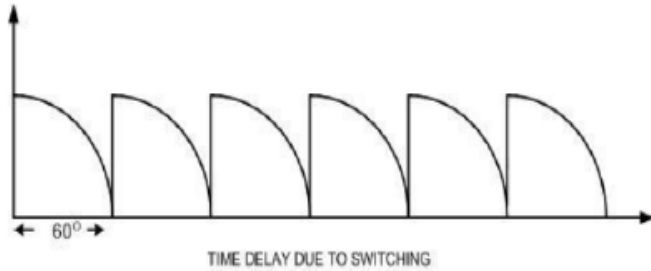


Figure 3. Output of three phase controlled rectifier.

Ripple will be six times the fundamental frequency. So the duration of each ripple will be 60 Degree.

Let for 50 Hz supply:

For 360 degrees, Time period $T = (1/50) = 0.02$ s.

For 60 degree, $t = (0.02 * 60)/360 = 3.3$ ms.

A change in converter firing angle occurs after every 60 degree. It's not instantaneous. That means a delay of 3.3 ms. It can have a maximum delay of 3.3 ms or a minimum of zero.

So, let us take an average $T_r = (3.3 \text{ ms} + 0)/2 = 1.7$ ms.

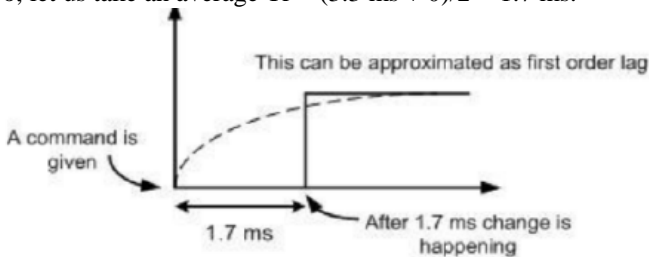


Figure 4. Ripples with 60 degree duration for 50 Hz waveform.

So, converter can be represented as a first order delay with a gain. So, converter can be represented as first order lag with some gain K_t .

$$\frac{K_t}{1 + STt}$$

IV. CONTROLLERS DESIGN

The controllers used in closed loop system to provide a very easy control and common technique of keeping motor speed at desired set point by continuously control of motor input. If the loads will increases then speed of the motor will decrease and the error will be negative. To compensate the speed, motor controller output should be increase and vice-versa. [3]

A. Designing of current controller:

We need to design of current controller because at the time of starting, back emf is zero (due to zero speed) that is during starting period large current flows through the motor.

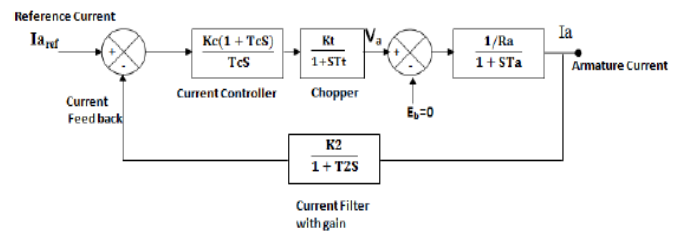


Figure 5. Block model of current controller design.

Transfer function of above block model is given as:

$$\frac{I_a(s)}{I_{aref}(s)} = \frac{K_t K_c (1 + ST_c) (1 + ST_a)}{R_a T_c S (1 + ST_t) (1 + ST_a) (1 + ST_2) + K_t K_c K_2 (1 + ST_c)} \quad (4.1)$$

Here, T_c (Current Controller Parameter) can be varied as when required. T_c should be chosen such that it cancels the largest time constant in the transfer function in order to reduce order of the system. Therefore the response will be much faster. So $T_c = T_a$. [3][9] Put the value in above equation (4.1), we get

$$\frac{I_a(s)}{I_{aref}(s)} = \frac{K_o (1 + ST^2)}{\delta S^2 + S + K_o K_2} \quad (4.2)$$

Then

$$K_c = \frac{R_a T_a}{2\delta K_t K_2}$$

The value of K_c and K_o put in equation (4.2) then we get:

$$\frac{I_a(s)}{I_{aref}(s)} = \frac{1/K_2}{1 + 2\delta S} \quad (4.3)$$

B. Designing of speed controller:

The block model of speed controller design is given below:

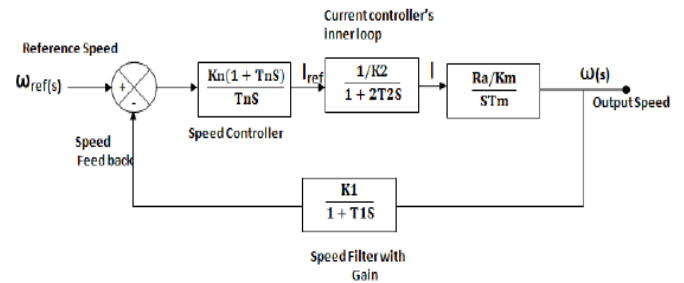


Figure 6. Block model of Speed controller design.

Transfer function of above block model is given as:

$$\frac{\omega(s)}{\omega_{ref}(s)} = \frac{K_n R_a (1 + ST_n) (1 + ST_1)}{T_n K_2 K_m T_m S^2 (1 + 2\delta S) (1 + T_1 S) + K_n R_a K_1 (1 + T_n S)} \quad (4.4)$$

To cancels the largest time constant of the transfer function so $T_n = 2\mu\delta$ then, Transfer function of above block model is given as:

$$\frac{\omega(s)}{\omega_{ref}(s)} = \frac{K_n R_a (1 + ST_1)}{T_n K_2 K_m T_m S^2 (1 + T_1 S) + K_n R_a K_1} \quad (4.5)$$

In above transfer function, the S term is absent. So that damping constant (ζ) will be zero. Due to this the system will be oscillatory and unstable. To optimize this we must get transfer function whose gain is close to unity. For this purpose the MODULUS HUGGING APPROCH is used. [2][3][5].

V. SIMULINK MODEL OF CLOSED LOOP SPEED CONTROL OF SEDC MOTOR USING CONTROLLED RECTIFIER

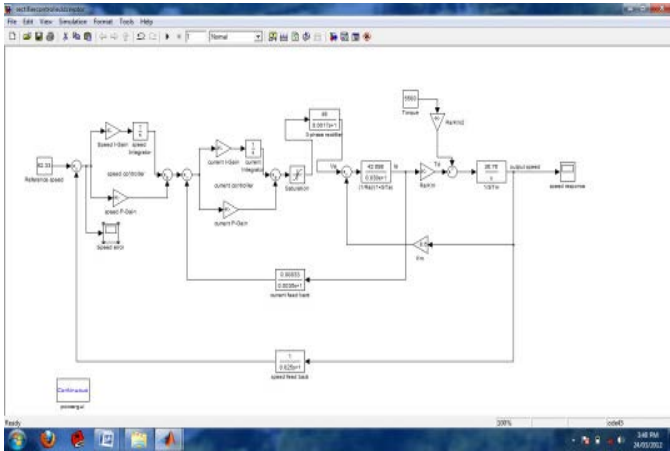


Figure 8. Simulink model of closed loop speed control of SEDC Motor.

VI. SIMULATION RESULTS

The simulation results of different speed and load torque:

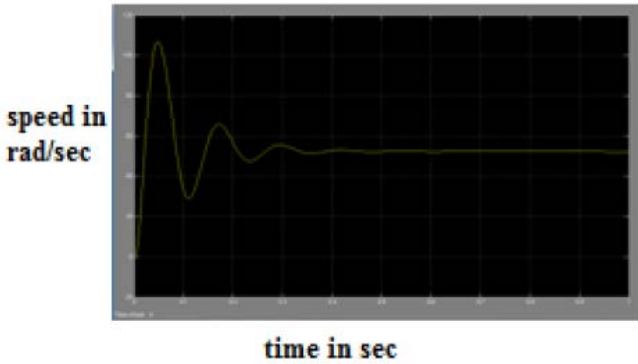


Figure 9. Speed response at rated speed and rated load torque

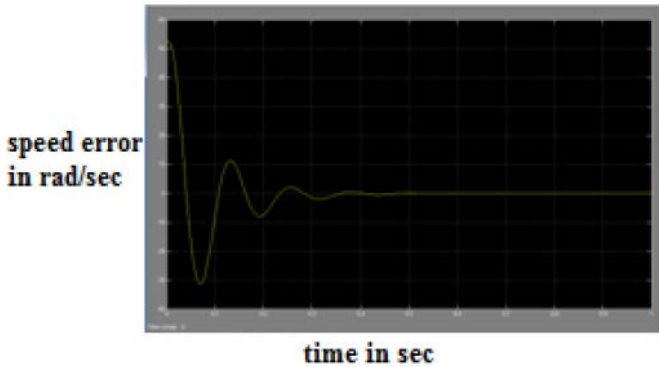


Figure 10. Error in speed response at rated speed and rated load torque

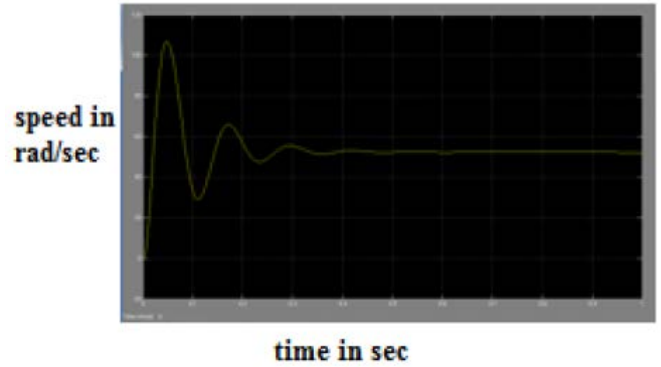


Figure 11. Speed response at rated speed at half of rated load torque

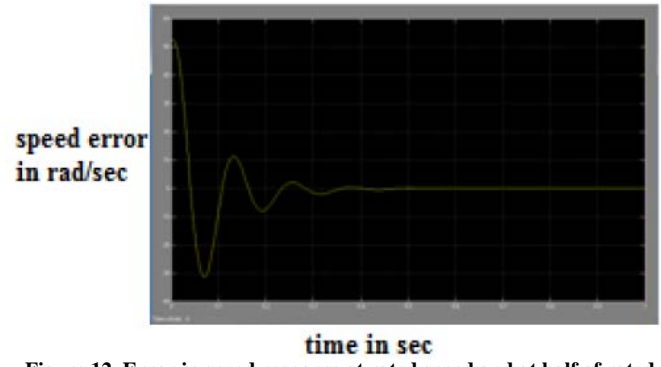


Figure 12. Error in speed response at rated speed and at half of rated load torque

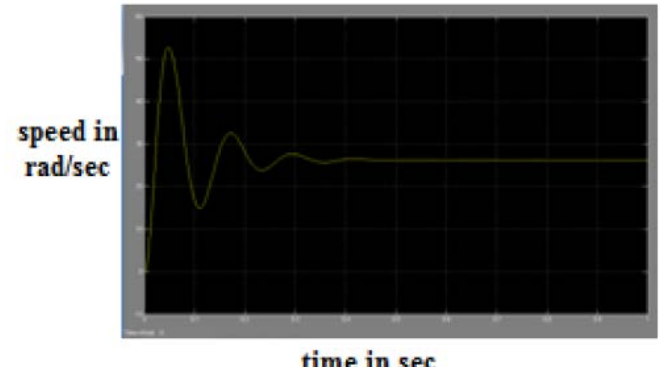


Figure 13. Speed response at half of rated speed and at rated load torque

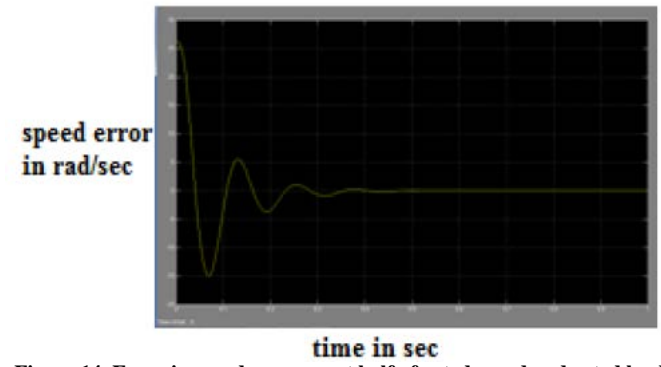


Figure 14. Error in speed response at half of rated speed and rated load torque

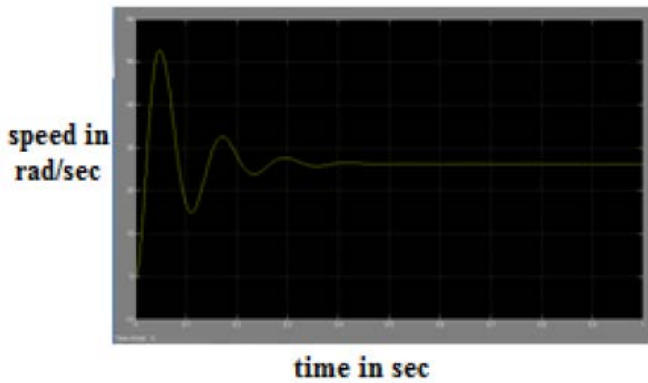


Figure 15. Speed response at half of rated speed and half of rated load torque

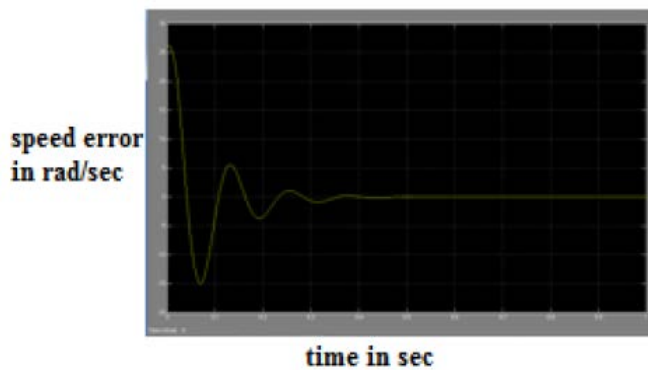


Figure 16. Error in speed response at half of rated speed and half of rated load torque

VII. CONCLUSION

This paper presents numerical demonstrating of shut circle speed control of dc engine utilizing three stage controlled rectifier. For stable operation of SEDC engine, the outlining of speed controller is finished utilizing Modulus embracing approach. By this approach the pick-up of framework progresses toward becoming solidarity. The recreation comes about are gotten in the wake of planning of shut circle framework. From the reproduction result we watched that the speed of SEDC engine is consistent at the reference speed which is evaluated or underneath the appraised speed of engine and furthermore watched that the speed blunder is set to be zero. The framework's reaction demonstrates the quick ascent time, quick setting time and additionally quick recuperating time.

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