

Comparative Analysis of Dual, Quad and Octa Element Patch Array Antenna

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Abstract

Antenna engineering and communication systems always compliment with each other. In wireless communication systems always an antenna with appreciable performance is a desired one and it should be compact as well as flexible in nature. Rectangular microstrip patch antenna with single element can satisfy the above mentioned criteria, but it is not suitable for the radar communication. In view of the above mentioned facts, this endeavor purely concentrates on the design of the antenna array with dual, quad and octa patch by using edge feeding technique in three different methodologies. The 2, 4 and 8 element antenna array is designed and their characteristics are compared with each other. The operating frequency for this design hangs around 10GHz. Rogers RT/ Duroid 5880 with a dielectric constant of 2.2 and loss tangent of 0.009 has been chosen as a dielectric material to carry out the design and HFSS is the platform for the implementation.

Keywords: Antenna array, Directivity, Edge fed, Gain, HFSS, Microstrip patch antenna, Rogers RT Duroid.

1. Introduction

An antenna is a transducer that converts the radio frequency fields into alternating currents or vice versa. It also acts as an impedance matching device between the source and load. The equivalent network of a transceiver can also be analyzed in the form of a network which satisfies the basic network theorems. As the antenna is subjected to radiate power to longer distances, it has a folded structure [1-2]. To measure the distance of the ships and to provide navigation at sea shore in marine radars, asymmetrical sum patterns are useful. These patterns are very helpful in point to point communication. [3-5].

The Microstrip Patch Antenna is a single-layer design which consists generally of four parts (patch, ground plane, substrate, and the feeding part). Patch antenna can be classified as single – element resonant antenna [6]. Once the frequency is given, everything (such as radiation pattern input impedance, etc.) is fixed. The patch is a very thin ($t \ll \lambda_0$, where λ_0 is the free space wavelength)

radiating metal strip (or array of strips) located on one side of a thin non-conducting substrate, the ground plane is the same metal located on the other side of the substrate. The metallic patch is normally made of thin copper foil plated with a corrosion resistant metal, such as gold, tin, or nickel. The substrate layer thickness is 0.01– 0.05 of free-space wavelength.

Among all the antennas, microstrip patch antennas are widely used in various applications because of its low profile, low cost, light weight and ease of installation with the RF devices. The most used Microstrip antenna is a Rectangular Patch because of ease of analysis and fabrication [7]. The key note in the antenna design is to choose a dielectric material and it should be given a higher priority because the geometry of the aerial is based on the value of the dielectric constant. For a high efficiency system, the insulating material with lower value of dielectric constant is preferred. Hence in this work, Rogers RT/ Duroid with a dielectric constant of 2.2 has been chosen. Figure 1 shows a microstrip patch antenna.

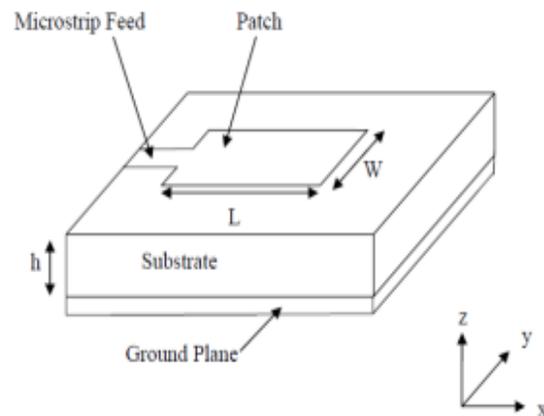


Fig. 1 Rectangular microstrip patch antenna

2. Antenna Array

Higher values of the antenna gain cannot be achieved with a single element. An antenna array is a ultimate solution to make the aerial as a competent one in terms of gain and directivity. Antenna array is the periodic arrangement of the similar type of conducting elements. All the elements in the array are isolated physically but there are connected electrically due to the fields associated in between them. Basically antenna arrays are classified as linear, phased and binomial arrays. In any array system, the total field pattern is always the algebraic sum of the patterns produced by each element.

As forementioned need for a customizable, flexible and small broadband system poses a problem not easily solved by a single element antenna. Monopulse techniques is one of the way to resolve the issue at an expense of limited flexibility in terms of both bandwidth and size. Modelled characteristics antenna can also be made utilized to meet this issue, but they always lag in the flexibility required and the spacing between each element should be a variable one.

An alternate solution is the phased array, which can provide similar gain and directivity characteristics without any restrictions on bandwidth and size. Phased arrays are also easily customizable to meet the spatial restrictions of the elements and it can allow all the components of the array located sparsely which in turn can improve the angular resolution [8]. Modern antenna configuring techniques permits the production of a highly compactable wideband antenna with any effect on the spacing.

3. Design Equations & Method of Analysis

Multiple methods were present in the analysis of microstrip patch antenna, among which the popular one is transmission line model. In which we assume that the conducting patch itself act as a transmission line or part of a transmission line. Transmission line model represents the antenna by two slots, separated by a low impedance transmission line of length L [9]. The results obtained through this model are good enough to design the antenna. Microstrip transmission line model can analyzed in two different cases. $W/h < 1$ i.e, narrow strip line and $w/h \gg 1$ and $\epsilon_r > 1$ i.e, a wider transmission line. The effective dielectric constant is given by the following equation.

$$\epsilon_{\text{reff}} = \frac{\epsilon_r + 1}{2} + \frac{\epsilon_r - 1}{2} \left[1 + 12 \frac{h}{W} \right]^{-1/2} \quad (1)$$

The effective dielectric constant is the function of the resonating frequency.

$$f_r = \frac{1}{2L \sqrt{\epsilon_{\text{reff}} \mu_o \epsilon_o}} \quad (2)$$

The width of the microstrip line is given as

$$W = \frac{\lambda_o}{2} \sqrt{\frac{2}{\epsilon_r + 1}} \quad (3)$$

The microstrip patch antenna looks longer than its physical dimensions because of the effect of fringing. The effective length therefore is differing from the physical length by ΔL . A very popular approximation to calculate the extension of the length of the patch is given by

$$\frac{\Delta L_{\text{eff}}}{h} = 0.412 \frac{(\epsilon_{\text{reff}} + 0.3) \left(\frac{W}{h} + 0.264 \right)}{(\epsilon_{\text{reff}} - 0.258) \left(\frac{W}{h} + 0.8 \right)} \quad (4)$$

To calculate the effective length, we add the length L to the extension of the length ΔL_{eff} .

$$L_{eff} = (L + 2\Delta L_{eff}) \tag{5}$$

The characteristic impedance of the microstrip line is given as

$$Z_0 = \frac{120\pi}{\sqrt{\epsilon_{reff}} \left(1.393 + \frac{W}{h} + \frac{2}{3} \ln\left(\frac{W}{h} + 1.444\right) \right)} \tag{6}$$

4. Design of a Single Element Patch Antenna

From the mentioned transmission line model equations, the dimension of the single element patch antenna are calculated and obtained as follows: Length of the patch 0.9cm, width of the patch 1.19cm, inset feed length 0.295cm, feed width of 0.243cm.

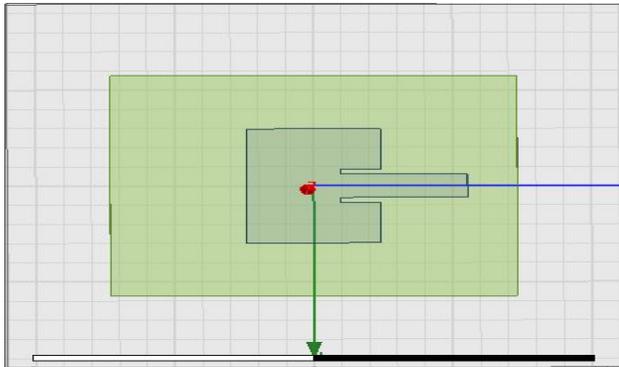


Fig. 2 Single element patch antenna

The performance of the single element patch antenna can be depicted from the following table 1.

Table 1: Performance of single element patch antenna

Parameter	Values
Return Loss	-17.96
Gain	8.1dB
Directivity	8.13dB
Beamwidth	71.08 ⁰

5. Design of a Dual Element Antenna Array

The dimensions of the two elements are similar to the dimensions of the single element. The feeding technique is edge fed, and it was applied in three different methodologies namely, individual, parallel and series. The separation gap between each element is $\lambda/2$.

In individual feed, the two elements lie on same plane and for each element, a separate feeding point is located. Here in this design two feed points are required.

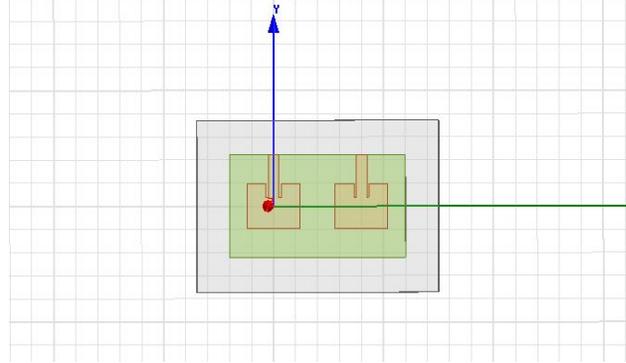


Fig. 3 Dual element array with individual feed

In parallel feed, the feeding to this array is designed through a T-network impedance matching network and a single feed point is enough to excite the array.

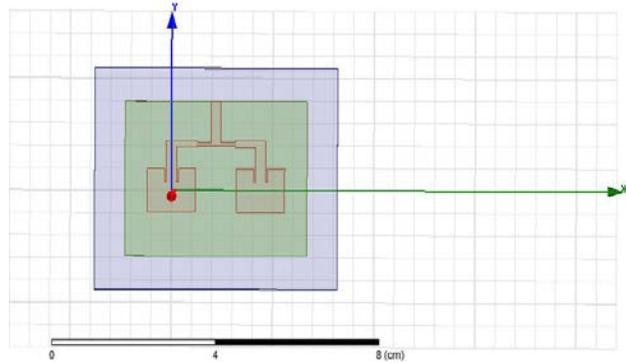


Fig. 4 Dual element array with series feed

In series feed, all the elements lie along a same line and each element is interconnected through a narrow feedline. In series feed, a single feed point is required to excite the two elements. Excitation is always given to the extreme patch element.

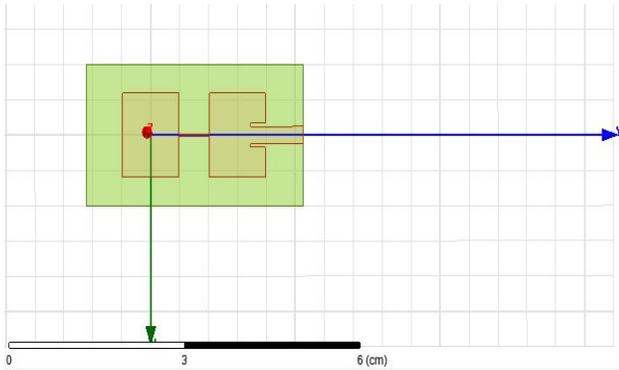


Fig. 5 Dual element array with parallel feed

Table 2: Performance of dual element antenna array

<i>Feed</i>	<i>Return Loss</i>	<i>Gain</i>	<i>Directivity</i>	<i>Beamwidth</i>
Individual	-19.7dB	10.6dB	10.63dB	40 ⁰
Parallel	-14.5dB	10.2dB	10.2dB	36 ⁰
Series	-15.5dB	9.62dB	9.7dB	49 ⁰

6. Design of a Quadruple Element Antenna Array

By considering the same dimensions of the single element and by modifying the position within the same plane, a quadruple element antenna array can be derived. Here for the four elements, feed points are required through which the excitation can be provided.[10].

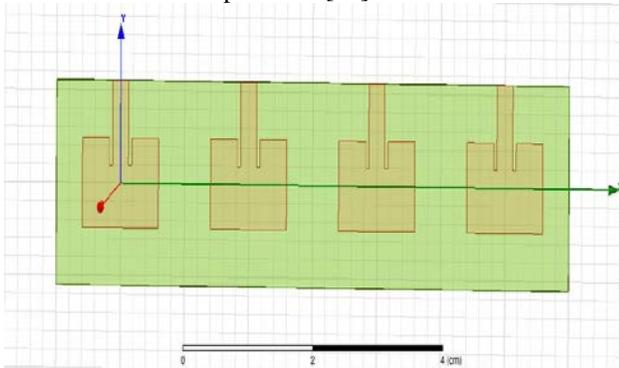


Fig. 6 Quad element array with individual feed

The same dimensions of the single element antenna were used here as well. The separation gap between all the patch elements is one half of its operating wavelength i.e., $\lambda/2$. Determining the location of the feed point is also an important task while designing the antenna [11].

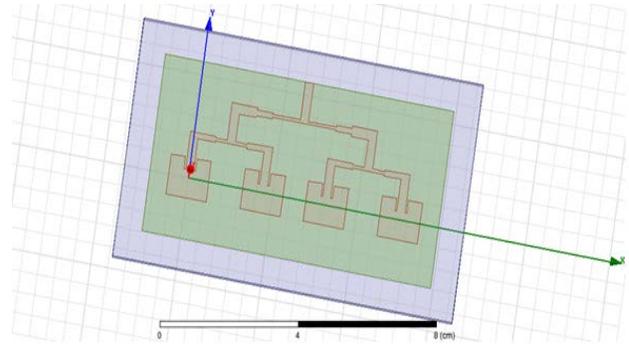


Fig. 7 Quad element array with parallel feed

The same dimensions of the single element patch antenna are also used in design of the 4 element antenna with series feed. The separation gap between two patches is $\lambda/2$. As the number of elements are increasing the dimensions of the substrate also increases.

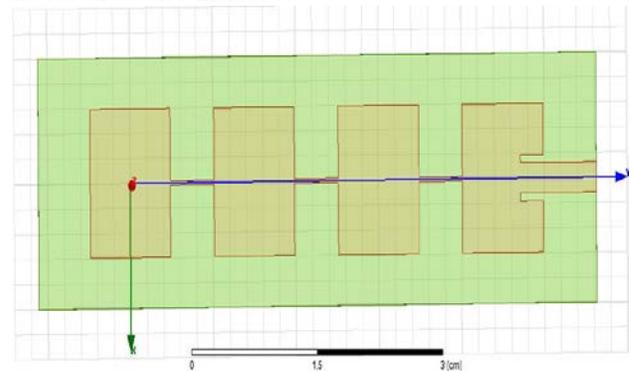


Fig. 8 Quad element array with series feed

The performance analysis of a quad element antenna array can be depicted from the following Table 2.

Table 3: Performance of quad element antenna array

<i>Feed</i>	<i>Return Loss</i>	<i>Gain</i>	<i>Directivity</i>	<i>Beamwidth</i>
Individual	-20.1dB	13.6dB	13.65dB	20 ⁰
Parallel	-27.5dB	13dB	13.73dB	17 ⁰
Series	-22.7dB	11.9dB	11.95dB	40 ⁰

7. Design of a Octa Element Antenna Array

The 8 element design of patch array antenna network is also utilizing the dimensions of the one element antenna. In octa element array system, all the 8 elements are provided with the individual feed by making sure that the feedline impedance resembles with the impedance of the single element antenna and 50ohm is the terminating line impedance (Z_0) [12].

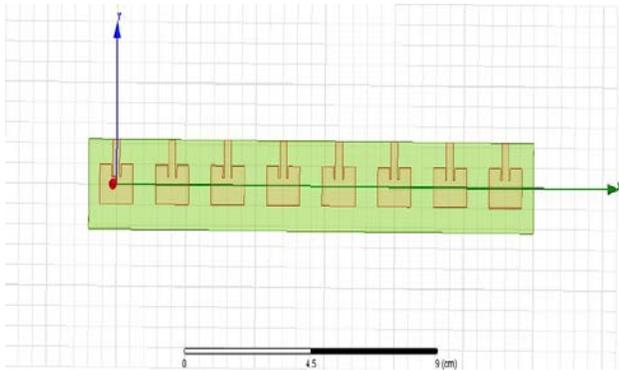


Fig. 9 Octa element array with individual feed

In 8 element antenna array, the feeding network is arranged in a parallel way. T-network is the basic configuration for the design of the feedline. Here 50ohm, 75ohm and 100ohm are the available line impedance and they can be chosen as per requirement.[13].

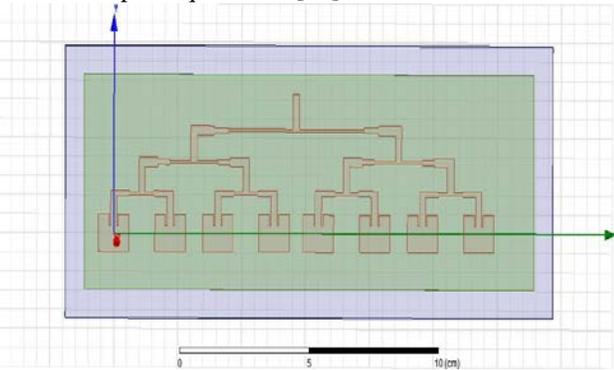


Fig. 10 Octa element array with parallel feed

Above the substrate all the 8 elements are placed serially and they are connected with each other through a narrow feedline. The feedpoint is located at the extreme patch and the excitation is given to it and all the remaining elements gets excited because of the narrow feedline with a terminating impedance of 50ohm. The placing between each element is maintained constant all through the design $\lambda/2$.

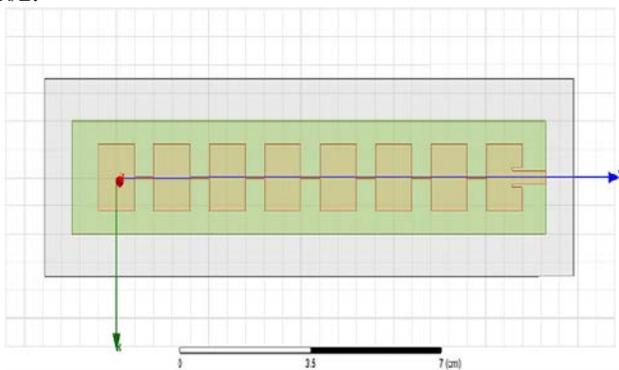


Fig. 11 Octa element array with series feed

The performance analysis of a octa element antenna array can be depicted from the following Table 3.

Table 4: Performance of octa element antenna array

<i>Feed</i>	<i>Return Loss</i>	<i>Gain</i>	<i>Directivity</i>	<i>Beamwidth</i>
Individual	-20.4dB	16.6dB	16.62dB	11 ⁰
Parallel	-18.8dB	16.5dB	16.5dB	9 ⁰
Series	-28dB	13.2dB	13.3dB	34 ⁰

8. Results And Discussions

The following section gives the comparison analysis and plots of the respective designs.

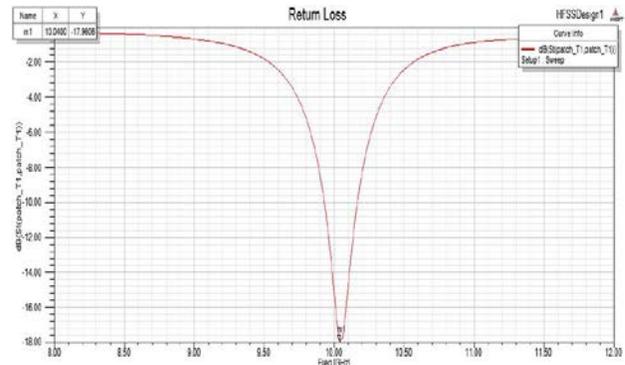


Fig. 12 Single element patch antenna

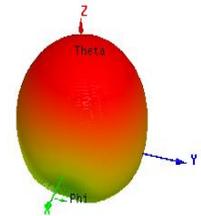
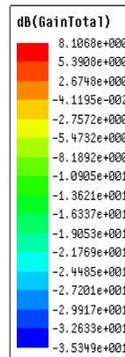


Fig. 13 Gain of single element patch antenna

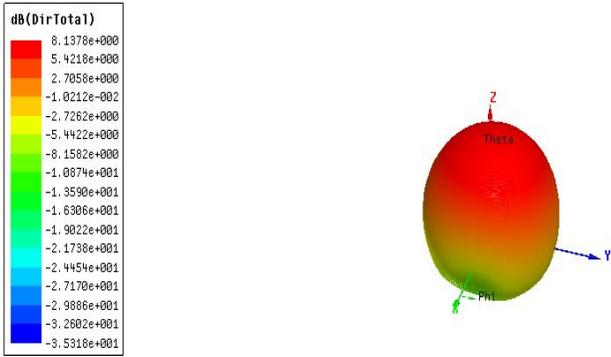


Fig. 14 Directivity of single element patch antenna

Fig. 17 Directivity of dual element array with individual feed

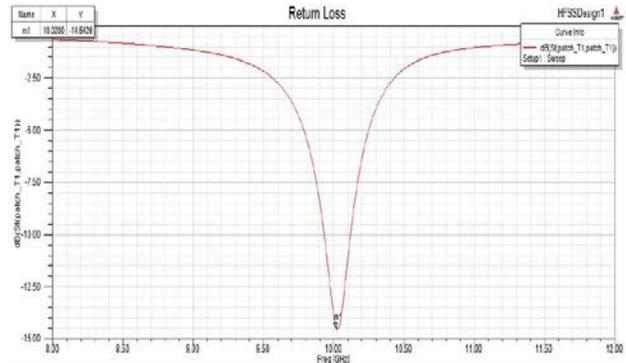


Fig. 18 Return loss of dual element array with parallel feed

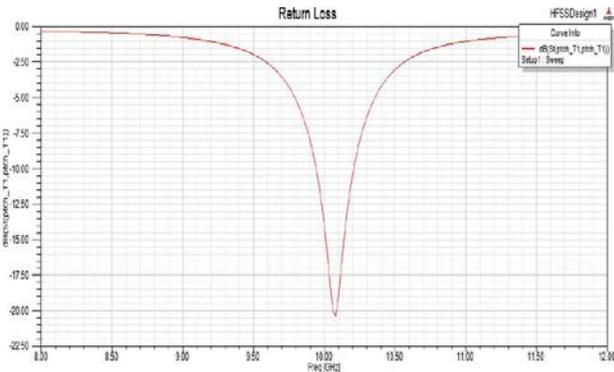


Fig. 15 Return loss of dual element array with individual feed

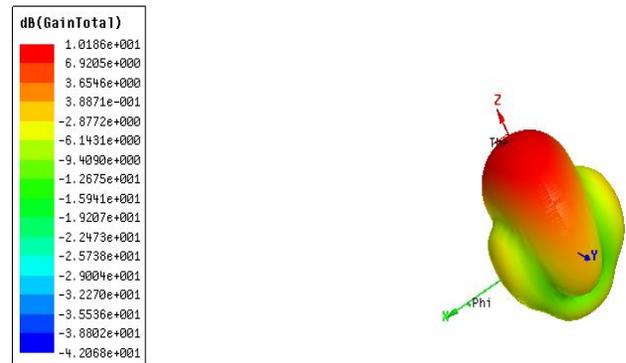


Fig. 19 Gain of dual element array with parallel feed

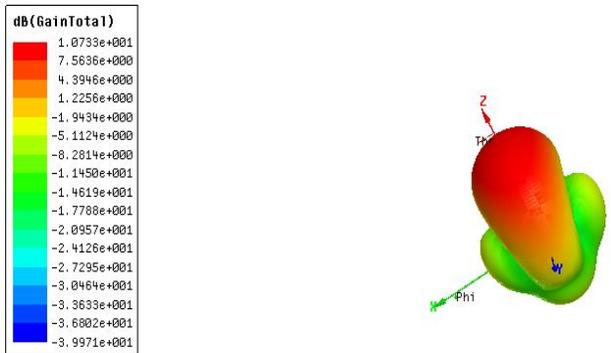


Fig. 16 Gain of dual element array with individual feed

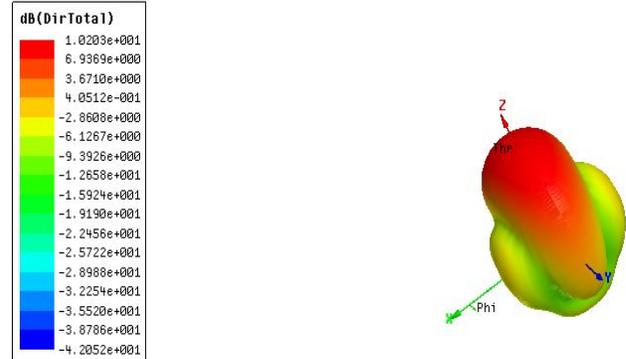
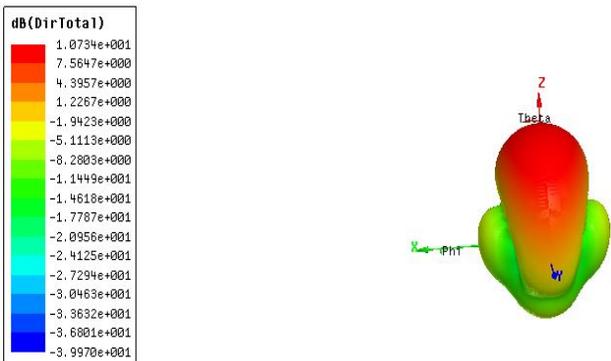


Fig. 20 Directivity of dual element array with parallel feed



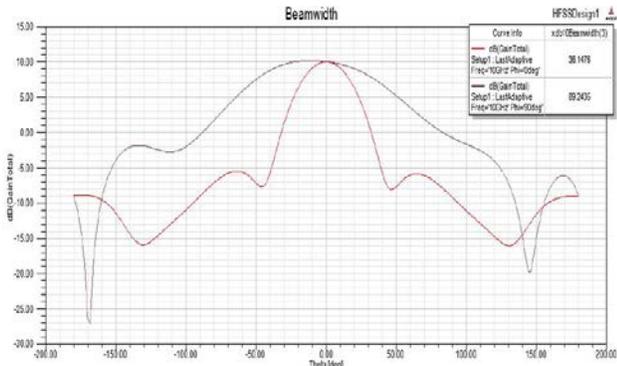


Fig. 21 Beamwidth of dual element array with parallel feed

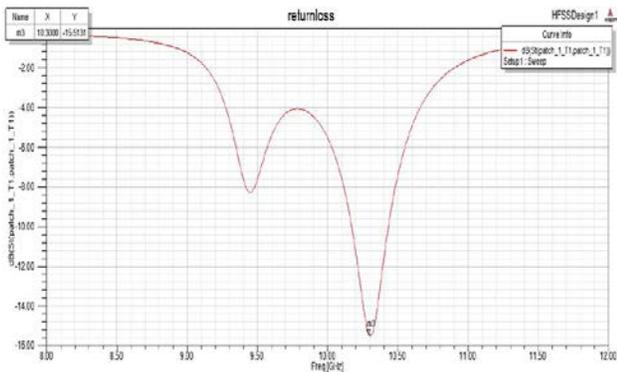


Fig. 22 Return loss of dual element array with series feed

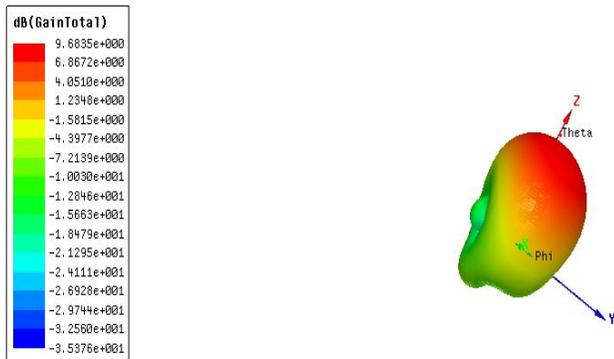


Fig. 23 Gain of dual element array with series feed

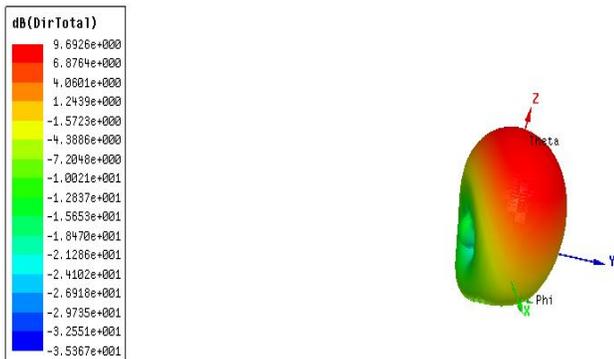


Fig. 24 Directivity of dual element array with series feed

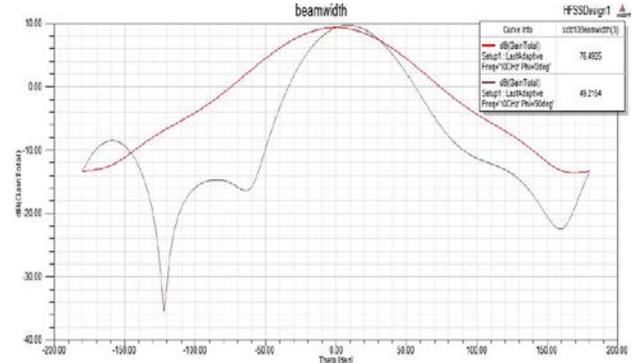


Fig. 25 Beamwidth of dual element array with series feed

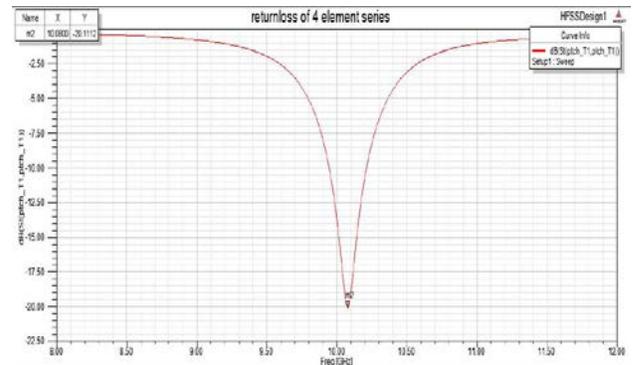


Fig. 26 Return loss of quad element array with individual feed

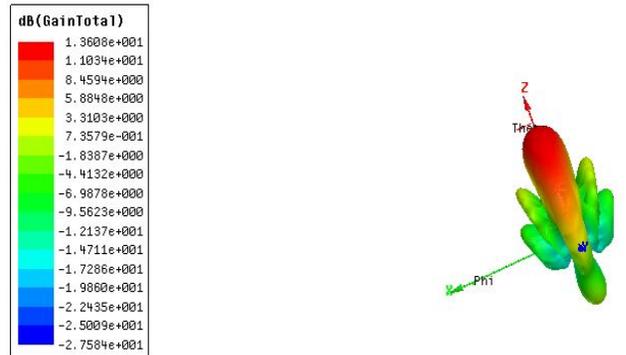


Fig. 27 Gain of quad element array with individual feed

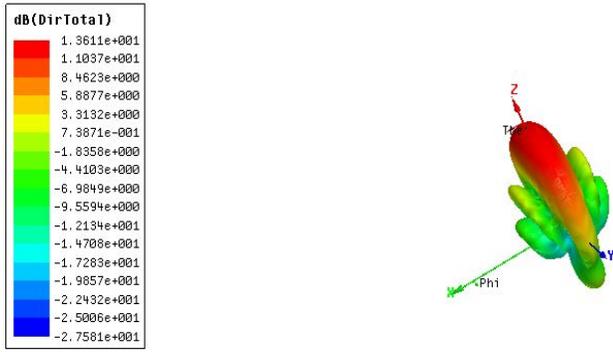


Fig. 28 Directivity of quad element array with individual feed

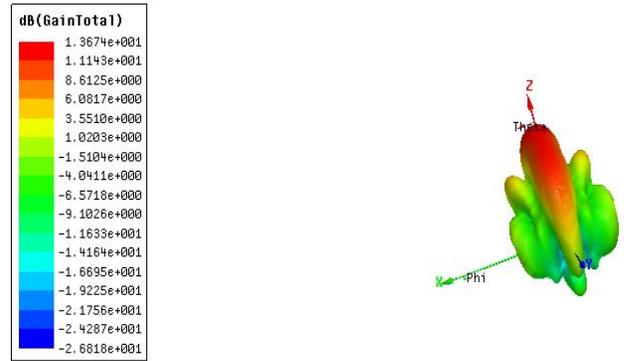


Fig. 31 Gain of quad element array with parallel feed

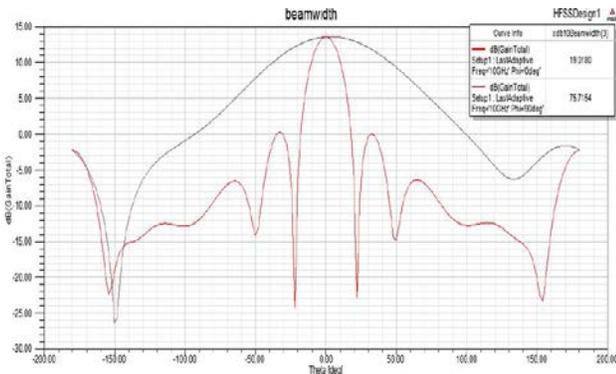


Fig. 29 Beamwidth of quad element array with individual feed

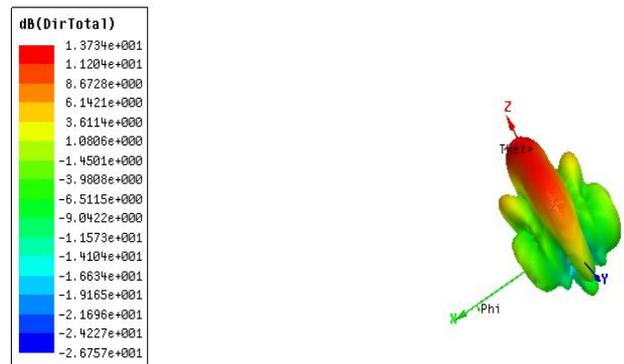


Fig. 32 Directivity of quad element array with parallel feed

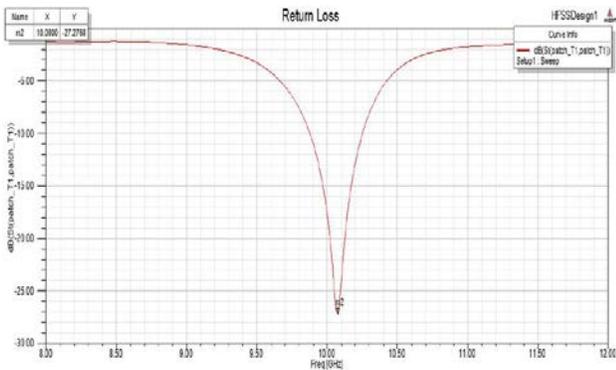


Fig. 30 Return loss of quad element array with parallel feed

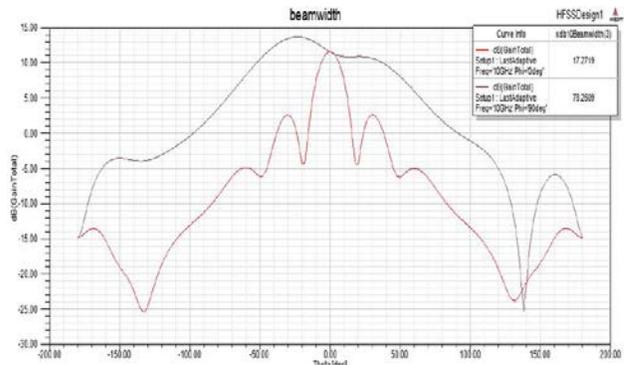


Fig. 33 Beamwidth of quad element array with parallel feed

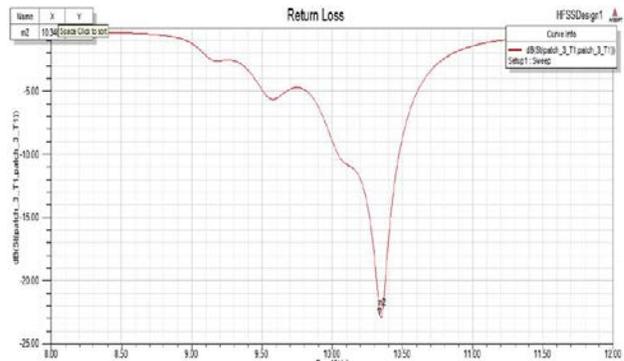


Fig. 34 Return loss of quad element array with parallel feed

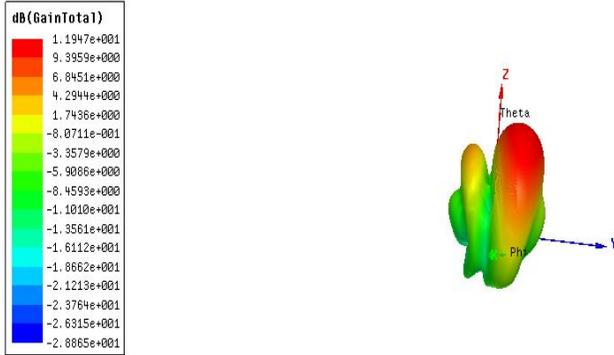


Fig. 35 Gain of quad element array with series feed

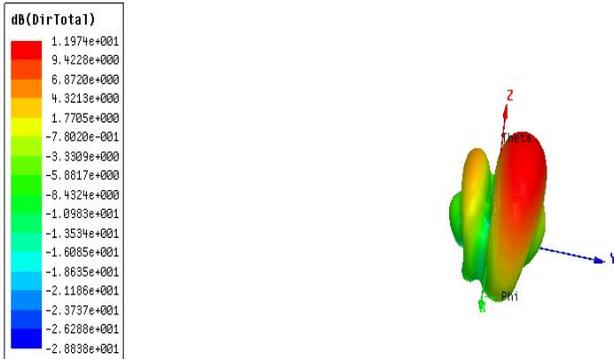


Fig. 36 Directivity of quad element array with series feed

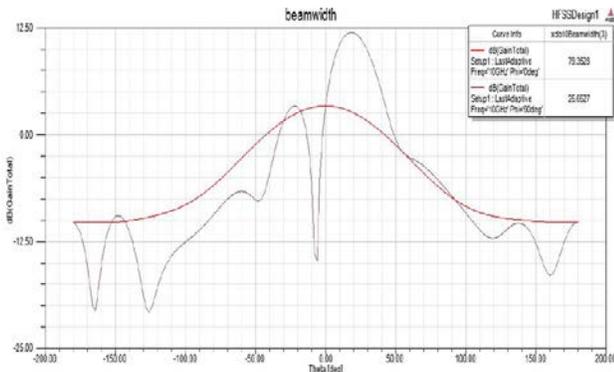


Fig. 37 Beamwidth of quad element array with series feed

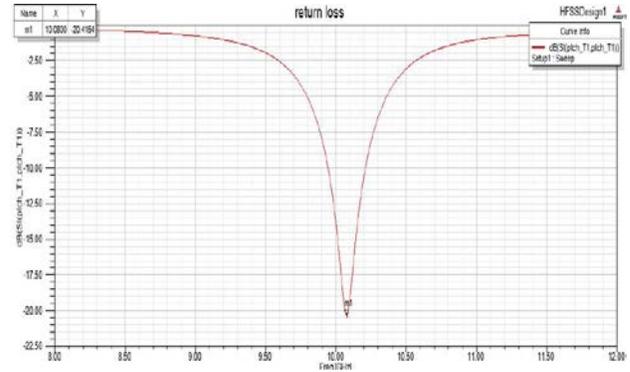


Fig. 38 Return loss of octa element array with individual feed

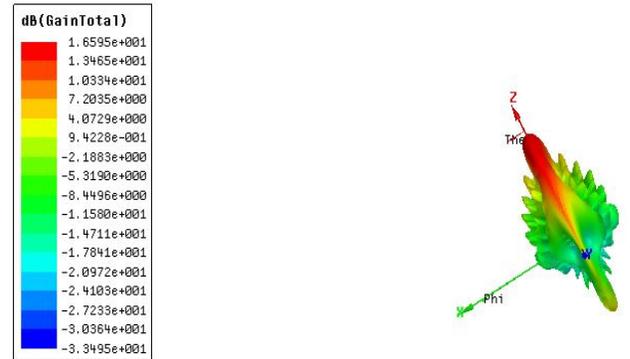


Fig. 39 Gain of octa element array with individual feed



Fig. 40 Directivity of octa element array with individual feed

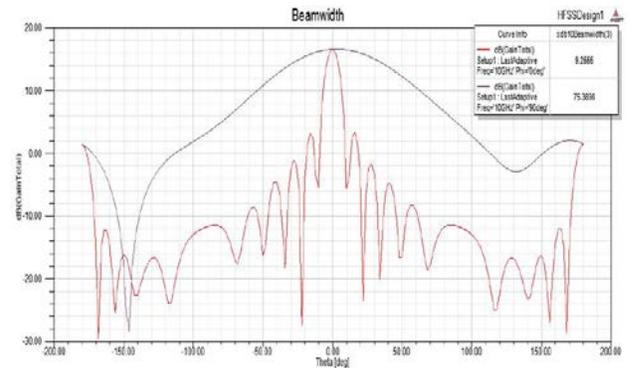


Fig. 41 Beamwidth of octa element array with individual feed

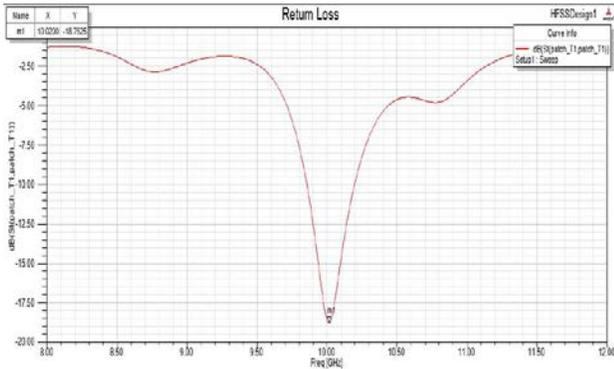


Fig. 42 Return loss of octa element array with parallel feed

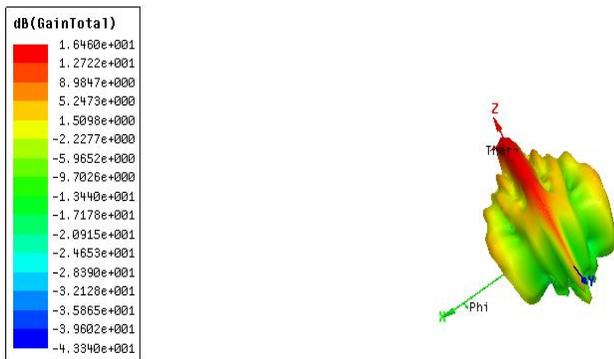


Fig. 43 Gain of octa element array with parallel feed

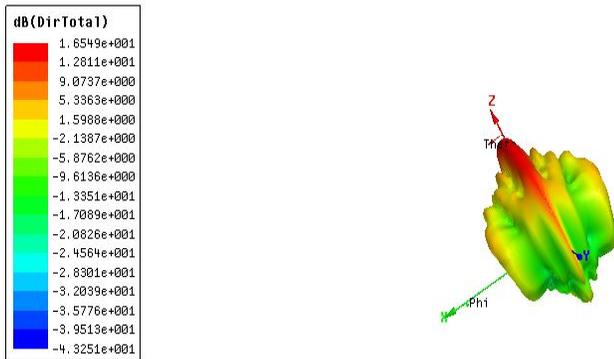


Fig. 44 Directivity of octa element array with parallel feed

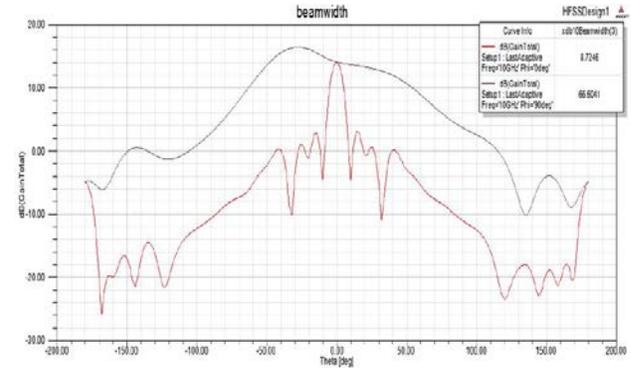


Fig. 45 Beamwidth of octa element array with parallel feed

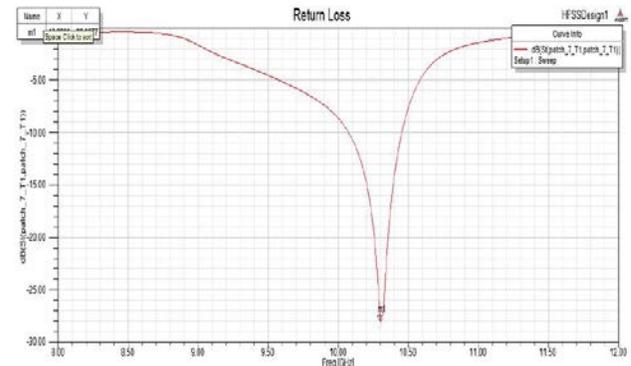


Fig. 46 Return loss of octa element array with series feed



Fig. 47 Gain of octa element array with series feed



Fig. 48 Directivity of octa element array with series feed

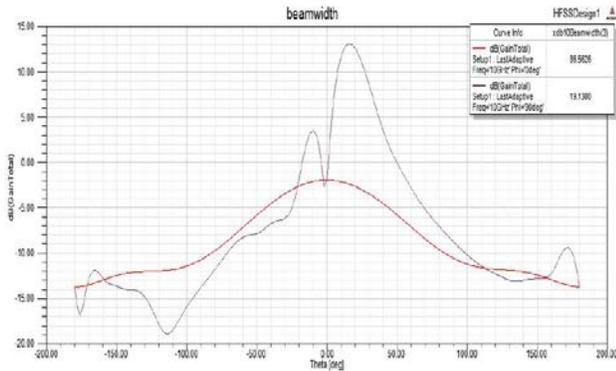


Fig. 49 Beamwidth of octa element array with series feed

Table 5: Overall performance analysis of antenna array

Parameter	Least Value	Enhanced Value	Design of enhanced value
Return loss	-18.8dB	-28dB	8 element series
Gain	16.6dB	9.62dB	8 element individual
Directivity	16.62dB	9.7dB	8 element individual
Beamwidth	9°	49°	8 element parallel

The designed array antenna whose central frequency is around 10GHz can be adopted into Radar applications because of its low beam width. Return loss is enhanced when the antenna is feeding in serial, and there is a variation in the value of return loss for parallel feed because of number of elements. Whereas is individual feed, the variation in the return loss also increases but it is negotiable. If the number of conducting elements in an array is increasing then the gain and directivity are also increasing. Hence it can be concluded that when compared to all three types of feeding methods, individual feed offers better results in terms of Gain and Directivity.

9. Conclusions

The designed array antenna whose central frequency is around 10GHz can be adopted into Radar applications because of its low beam width. Return loss is enhanced when the antenna is feeding in serial, and there is a variation in the value of return loss for parallel feed because of number of elements. Whereas is individual feed, the variation in the return loss also increases but it is negotiable. If the number of conducting elements in an

array is increasing then the gain and directivity are also increasing. Hence it can be concluded that when compared to all three types of feeding methods, individual feed offers better results in terms of Gain and Directivity.

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